

CAGE MOTOR SLOT HARMONICS CAUSED BY A MAIN MAGNETIC CIRCUIT'S DETERIORATION

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Abstract

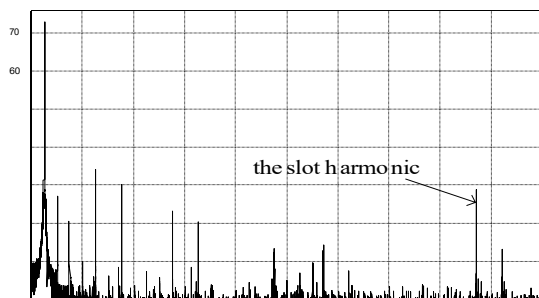
This research delves into the effects on cage motor phase current Fourier spectra brought about by fundamental MMF harmonic saturation of the main magnetic circuit. An analogy with the equivalence of a magnetic current is made use of. So, by considering the impact of all currents on the permeability of the main magnetic circuit, we may deduce when and why new bars appear in stator current spectra. The results of the measurements support our mental judgements.

I. INTRODUCTION

Currently, Fourier spectra of stator current are used to diagnose problems with cage motor rotors. Accurate measurements and predictions of those spectra are crucial to making an accurate diagnosis. This implies that the predictive mathematical model This motor's pole-pair number 'p' and rotor slot number 'N' determine the position of this supplementary bar [6]. This bar may be determined using a model that takes magnetic saturation into consideration [4, 6]. In this research, we propose a model and the numerical test results that prove it is capable of identifying these supplementary slot harmonics.

I. CAGE MOTOR

Saturation Modeling Using the Primary Magnetic Field A cage motor model is created using the co-energy function, which is segmented as $E_{co} > E_{mp} > E_{mh} > E$ to account for magnetic non-linearity. The and the precision of the measurement tools is essential. There magnetic circuit by the p-harmonic, which introduces non- includes the full spectrum of the MMFs of motor windings higher harmonics that disrupt the primary magnetic circuit. In the third There are still discernible quantitative distinctions between spectra. symbolizes the combined energy of potential leaking areas. It is model-based predictions and experimental motor measurements. Fig.1



$$\Theta = \frac{2i_m}{\pi p} \cos p(x - \alpha)$$

Assuming magnetic linearity, a mathematical model of this motor predicts just two bars, one at the main frequency of 50 Hz and the other at a slip-dependent frequency of $(35 + 34s) \cdot 50$ Hz (s - rotor slip), as shown in Fig.1 for $s=0,004$. Saturation is what causes the bars in a true spectrum, and their frequencies are multiples of wherein the stator voltages and currents are described using their 3-phase symmetrical components, and the cage mesh currents are described using their N -phase symmetrical components. The non-linear inductance arises in these equations.

50Hz, but there's also a rather tall bar out in the distance

$$L = \frac{3}{2} \cdot \frac{w^2 \cdot k^2}{A} \cdot \frac{1}{\partial E_{mp}} \quad (4)$$

100Hz with respect to the slot harmonic. The existence and $(w_s, k_{s,p}$ - stator phase turn number and winding factor) at the

following positions: in the matrix L^s at $(1, 1)$ and $(2, 2)$, in the matrix L^r at (p, p) and $(N - p, N - p)$. In the matrix M^s components appear. Beside a “classical” slot harmonic $(35 - 34 \cdot s) \cdot 50$ Hz, the new bars appear in the Fourier spectrum $(37 - 34 \cdot s) \cdot 50$ Hz and $(31 - 34 \cdot s) \cdot 50$ Hz, shown

appear non-linear terms: L at the position

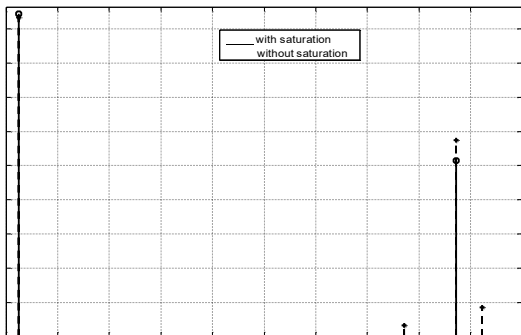
$(1, p)$ and in Fig.3 (at $s=0,004$).

he positions

$(2, N - p)$. The other elements of

Matrix representations of inductance in (3) are analogous to those in the magnetic linearity model [5]

I. Statistical Results



The function of permeability must be calculated.

$p = 30$ Co-Energy

MagNet6.0 20 has been used to compute the function.

Example motor FEM with a Fourier spectrum of 10 in Fig.1, we may use the function as a close approximation to the co-energy,

Fig3. Calculated Fourier spectrum of a phase current up to 2,54[kHz] of a motor $P_N=2$ MW, $U_N=6$ kV/Y, $p=1$, $N=34$ at $s=0,004$

$$E = 1.0635 \cdot (i) - 0.0635 \cdot (i) \quad (5)$$

VI. CONCLUSINS

The following may be said to wrap up the paper's considerations. When the primary magnetic circuit is saturated by the fundamental component of total MMF, additional slot harmonics might occur. Although this study presents a model that can quantitatively predict these harmonics, there is still a qualitative difference when compared to observation. The offered model does not, however, allow for the prediction of harmonics with frequencies greater than 50 Hz.

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